



Introduction to superconducting power cable systems

CE BRUZEK

Nexans France

ESAS Summer school –8-14 June 2016



Content

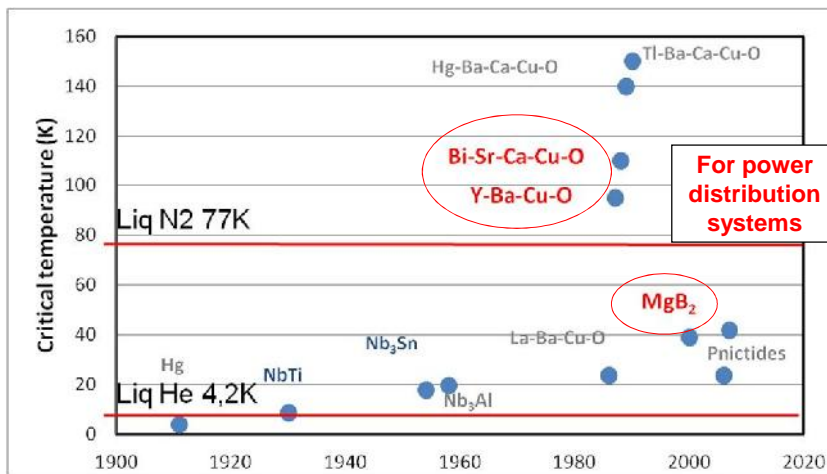
Introduction to superconducting power cable systems

1. The 5 main components
 - A. Superconducting tapes and wires
 - B. Cryogenic envelopes
 - C. Cryogenic machines
 - D. Cable designs
 - Warm dielectric
 - Cold dielectric
 - E. Terminations & Joints
2. Tests & Reliability
3. Some applications
4. HTS power cable system benefits

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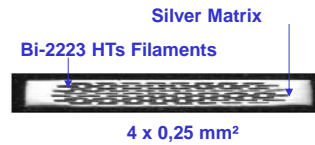
Superconducting tapes & wires (1)



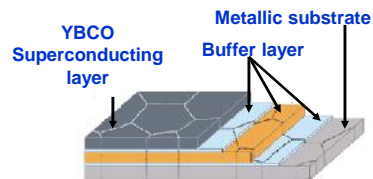
HTS tapes or MgB_2 wires for **current transportation**

2 kinds of tapes and 1 wire are available in long lengths

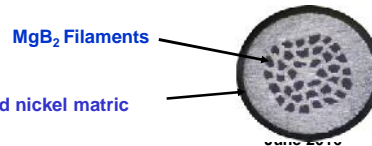
- 1st generation: Multifilamentary Bi 2223 tapes



- 2nd generation: YBCO Coated conductor



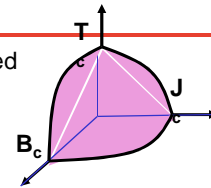
- Multi-filamentary wire ($T_{op} = 20-25K$)



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Superconducting materials lose their properties when the transported current exceeds the critical current density dependant on

- Magnetic field
- Temperature

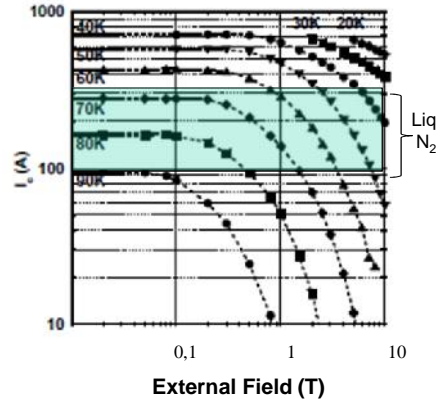
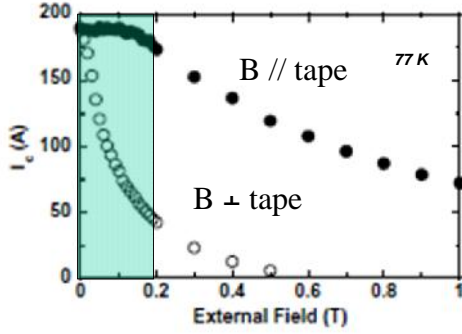


	Shape	Dimensions		Commercial performances	
		Width (mm)	Thickness (mm)	J_c (Amm^{-2}) @ 77K; self field ($A.cm^{-1}$)	Length (m)
Bi2223	Laminated tapes	4,5	0.32-0.36	140-150 A/mm^2 (475 – 500 A/cm)	< 2000 m
YBCO	Laminated NiW Tapes	4 to 12	0.3-0.45	100- 120 A/mm^2	< 500 m
	IBAD tapes		0.1	500- 700 A/mm^2 (500-650 A/cm)	
		<i>Diameter (mm)</i>		J_c (Amm^{-2}) @ 20 K ; 1T	<i>Length (m)</i>
MgB_2	Cylindrical wires	0.8 -1.5 mm		350	< 5000 m

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Bi2223 tapes at 65-77K



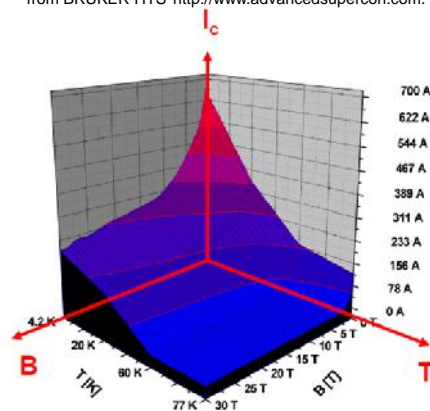
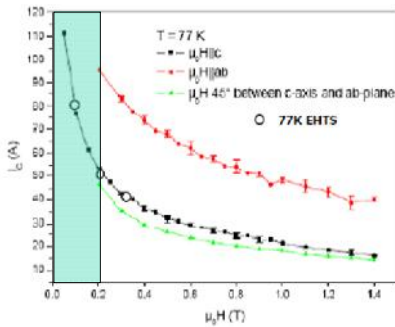
1. Keep the magnetic field parallel to the tape
2. Keep the magnetic as low as possible with a cable conductor relatively large $d > 25$ mm and moderate current of few kA

3. Operate in Liq N₂ the closest to 65K to benefit of a 2 factor on I_c

From Research, Fabrication and Applications of Bi-2223 HTS Wires edited by Ken Sato, World Scientific collection
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YBCO tapes at 65K-77K

from BRUKER HTS <http://www.advancedsupercon.com>.



1. Keep the magnetic field parallel to the tape
2. Keep the magnetic as low as possible with a cable conductor relatively large $d > 25$ mm and moderate current of few kA

3. Operate in Liq N₂ the closest to 65K to benefit of a 2 factor on I_c

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In superconducting tapes, AC Losses are mostly hysteresis losses that can be evaluated by:

$$H_a \gg H_p \quad P_{vol} = \frac{8}{3\pi} J_c d f B_a \quad [W/m^3]$$

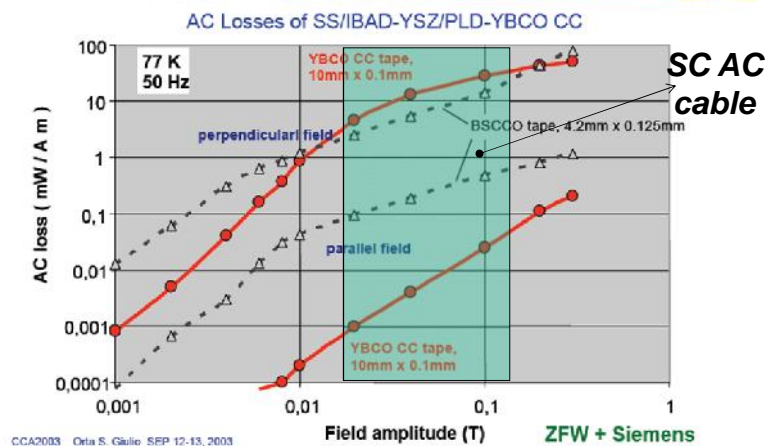
$$P_l = \frac{8}{3\pi} I_c d f B_a \quad [W/m]$$

d is the distance **perpendicular** to the applied field

High **transverse** field ac losses

PIT tapes : $l/e = 20$ ($l = 4 \text{ mm}$; $e = 0.23 \text{ mm}$)

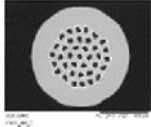
Coated Conductors : $l/e = 2000$ ($l = 4 \text{ mm}$; $e = 0.002 \text{ mm}$)



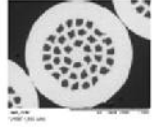
From P Tixador

Keep the magnetic field as low as possible and parallel to the tape

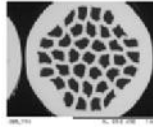
MgB₂ wires at 20-25K
A large variety of possible designs



Type 1
Diameter: 1 mm
•37 MgB₂ filaments
•Filling factor: 11.5%
•Nickel matrix, Monel sheath;
Niobium barriers;
Copper and Tin electroplated layer



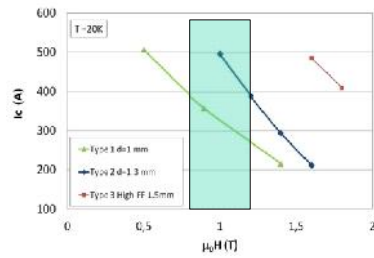
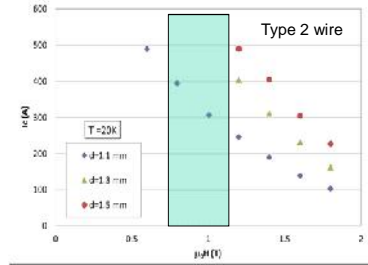
Type 2
Diameter: 1.33 mm
•36 MgB₂ filaments
•Filling factor: 17%
•Nickel matrix, Monel sheath



Type 3
Diameter: 1.5 mm
•37 MgB₂ filaments
•Filling factor: 30%
•Nickel matrix, Monel sheath

1. For high ampacity DC cable > 10kA
2. Keep the magnetic field around 1T
3. Small cable conductor diameter <15 mm to use the smallest cryogenic envelope

From Columbus SPA <http://www.columbusuperconductors.com>



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Typical cabling machine



Rotating pay off

Cabling point (die)



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Handling laminated 1G tape at room temperature for cabling operations

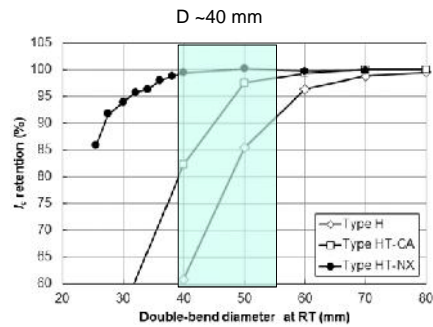
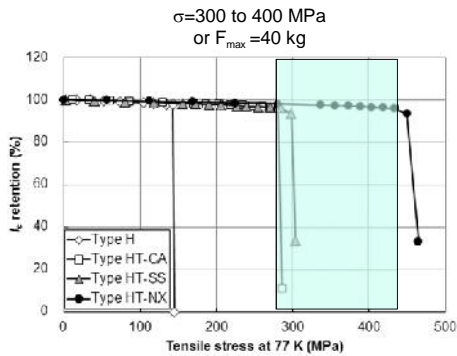
Different possible reinforcements

1. CA: copper alloys
2. SS: stainless steel
3. NX: nickel alloys



HT-CA tape

- width: approx. 4,3 mm
- thickness: approx. 0.3 mm



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Handling 2G tapes at room temperature for cabling operations

◆ Mechanical properties:

- ✓ Average thickness: 0.36 - 0.44 mm
- ✓ Minimum width: 4.24 mm
- ✓ Maximum width: 4.55 mm
- ✓ Minimum double bend diameter (RT): 35 mm
- ✓ Maximum rated tensile stress (RT): 200 MPa
- ✓ Maximum rated wire tension (RT): 20 kg
- ✓ Maximum rated tensile strain(77K): 0.3%



◆ Cabling reliability:

- ✓ Designed for cabling on a wide range of formers with tight pitch and large back tension.
- ✓ Durable in pressure cycled liquid nitrogen, including splices and joints



From American superconductors <http://www.amsc.com>

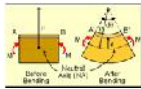
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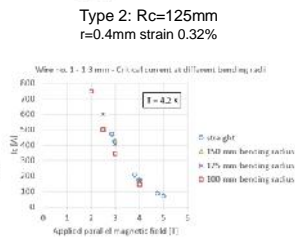
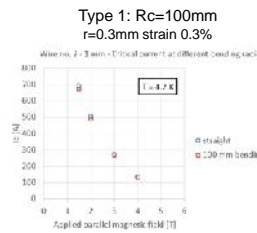
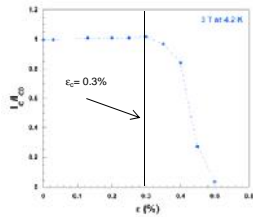
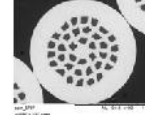
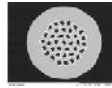
Handling MgB₂ wires at room temperature for cabling operations

Mechanical properties:

- Maximum rated tensile stress (RT): 150 MPa Fmax= 15-20 kg
- Maximum rated tensile strain(77K): 0.3%
- Minimum bending radius (see below)



$$\epsilon = \frac{A'B' - AB}{AB} = \frac{y}{\rho}$$



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Courtesy to Cern

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To maintain the low temperature and to transport the cryogenic fluids



- 1. Corrugated inner tube
- 2. Low-loss spacer
- 3. Vacuum space
- 4. Multilayer superinsulation
- 5. Corrugated outer tube
- 6. PE jacket (optional)



Simple envelope

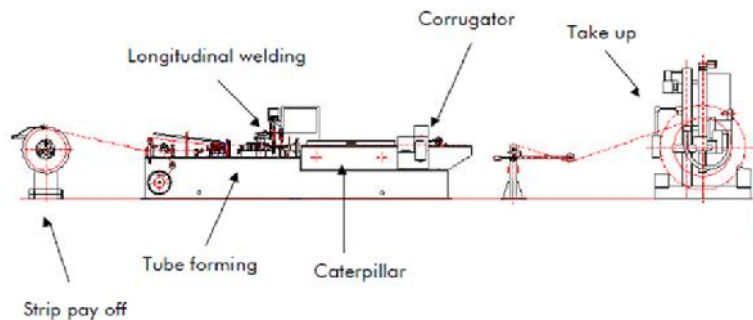
Double envelope with thermal shield for MgB₂

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Tube with shape & longitudinal welding process

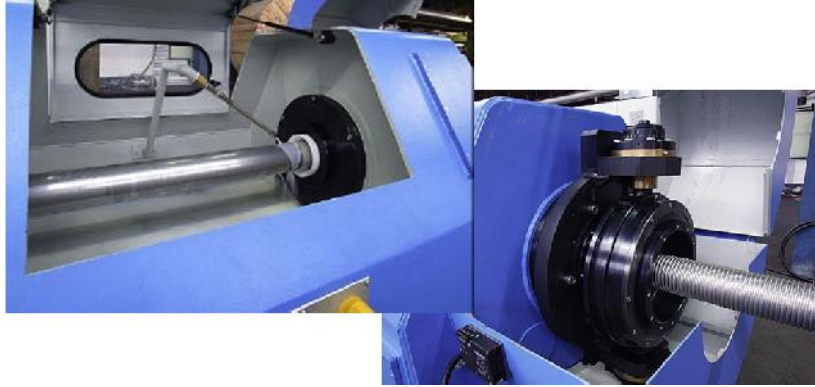
- Tube length are kilometric depending on
 - ◆ The strip length
 - ◆ The tube diameter



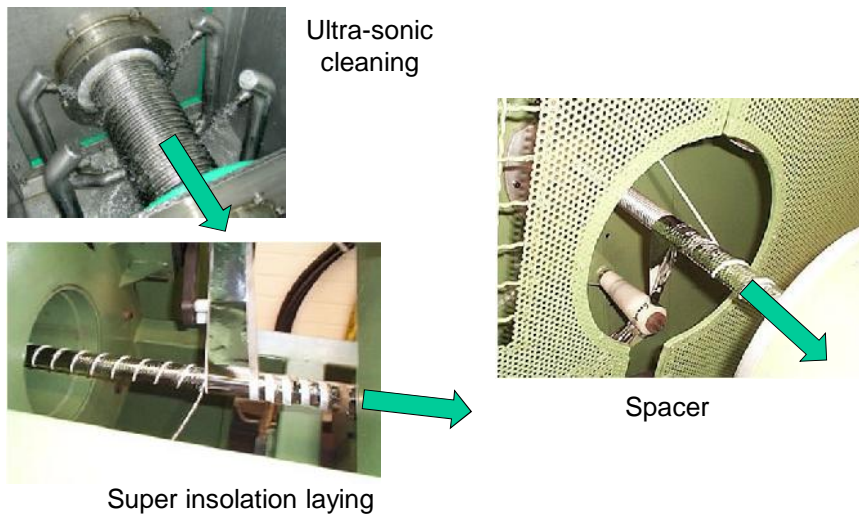
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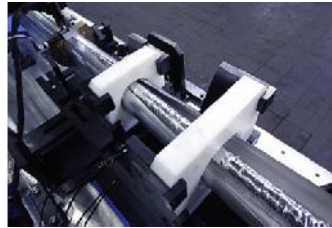
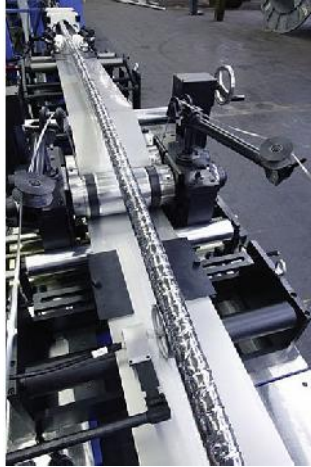
Corrugation of tubes (Flexibility)



Thermal insulation (*super-insulation and spacer*)



Outer tube shaping & welding



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1. Envelops are flexible (corrugation)
2. Life time
 - Experience of more than 20 years in progress...
3. Maintenance
 - ◆ Monitoring of vacuum level in operation
 - ◆ Crack location by non destructive controls (ultrasonic or Acoustic emission..)
4. Piece lengths from 250 m up to 1000 m depending on the diameter
 - Limitation: Ground transportation of the spools...
 - but low losses cryogenic couplings (bayonet) already exist



L H2 Coupling

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Thermal heat load depending on:

1. Envelop diameter
2. The number of super insulating layers
3. The gap between the inner and the outer tubes
4. The quality of vacuum

Heat inlet can be significantly **locally** increased when the cryo-envelope is **bent** or **perpendicularly pressed**

Models	2 walls					4 walls*		
	Small		Medium		Large	Small	Medium	Large
Int /Ext Dia Meter (mm) (Shield) *	14/34	21/44	39/66	60/110	75/125	21/44 + (60/110)*	39/66 + (90/147)*	75/125 + (147/220)*
Bending radius (Several bends) (m)	0.6	0.7	1.1	1.8	2	2	2.5	3
Heat inleak at T _{op} /Shield* (W.m ⁻¹)	0.4	0.6	1	1.2	1.4	0.07/1.2*	0.12/1.5*	0.3/2*
Weight (kg.m ⁻¹)	0.5	0.8	1.7	4	6.7	5	7.5	10

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Introduction to superconducting power cable systems

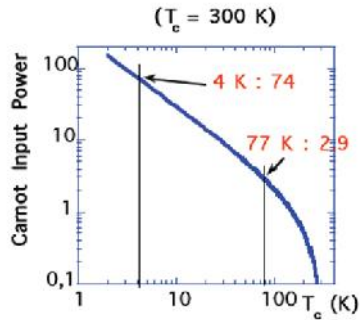
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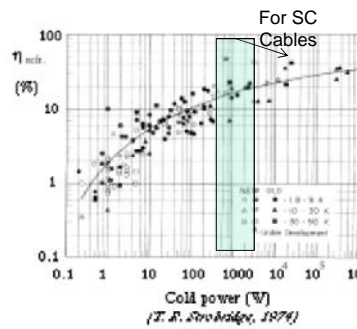
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Energetic cost

$$\frac{W_{\min}}{Q} = \frac{1}{\eta_f} \frac{T_o - T_c}{T_c}$$



From P Tixador



1W at 77K needs 10 to 25 W at RT
 1 W at 20 K needs 100 to 140 W at RT

Cryogenic machines (2)

1. To recover the cold power and the cryogenic fluid pressure
2. To circulate the cryogenic fluids

Large number of machines are commercially available from small to large cold power production to work in **close loop**



Ex Gifford Mc-Mahon machines

Cold power: up to 500W at 70K
 and 60W à 20K



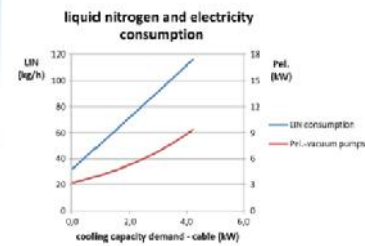
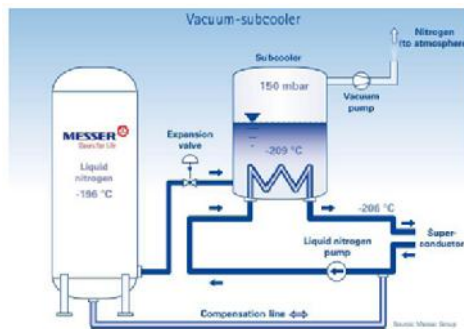
Ex: Turbo Brayton machines

Cold power: from 5kW to 30 kW at 70K
 and up to 5 kW at 20K

Also possible to use **open loop system** when LN₂ delivery on site is possible

Benefit: Use liquefied N₂ as primary cooling source

Example: Messer system at Ampacity Essen site



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Principle

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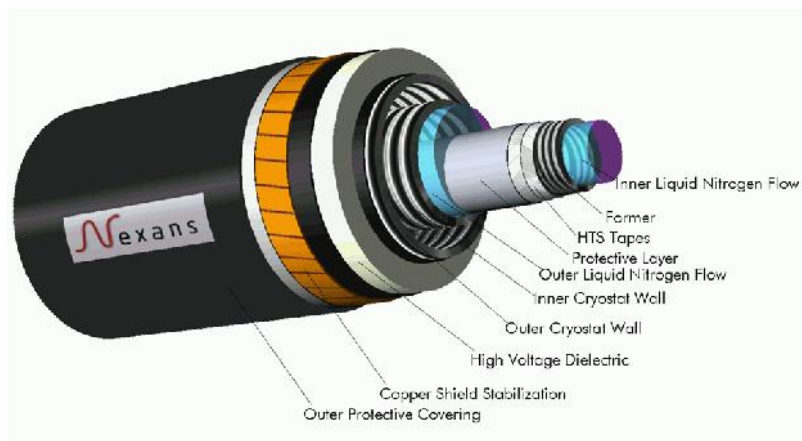
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- Cable: **Transport the power from one termination to an other**
 - High Currents and voltages management with the lower losses
 - 2 solutions for high voltage management:

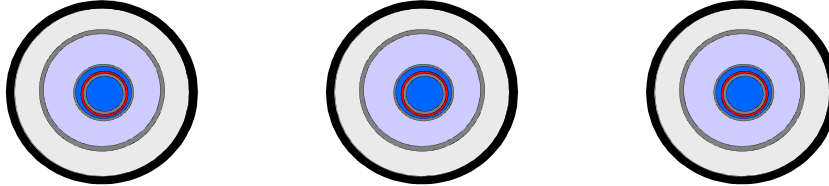
1. Dielectric applied to the external envelope => **Warm dielectric design**

Dielectric material applied on the external Envelope

extruded PE



3 separated phases

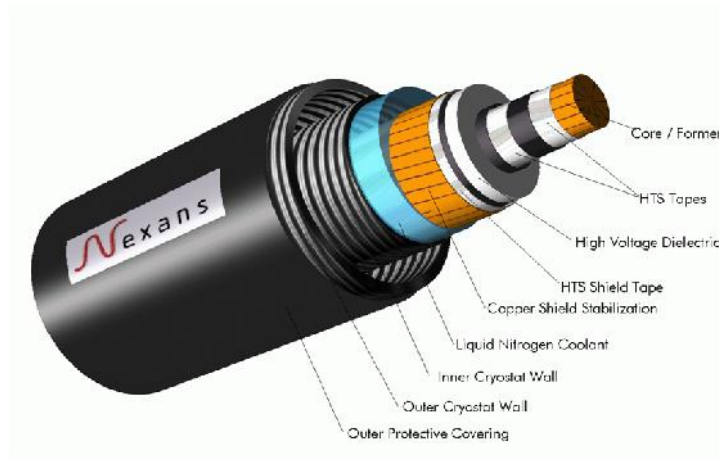


- Magnetic field from one phase affect the others
- Needs to separate the 3 phases
- Difficult to manufacture joints

Not realistic for long length power link

- Cable: Transport the power from one termination to an other
 - High Currents and voltages management with the lower losses
 - 2 solutions for high voltage management:
 1. Dielectric applied to the external envelope ⇒ Warm dielectric design
 2. Dielectric inside the inner envelope ⇒ Cold dielectric design

1. Fault tolerant design



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2. Fault limiting design



Constraints:

1. Only possible with 2G tapes
2. Needs more tapes to have an acceptable operating current/critical current ratio
3. Amount of fault current limitation depends on cable length and voltage level (about 10 V/m are needed)
4. Parallel paths of the grid need to be present

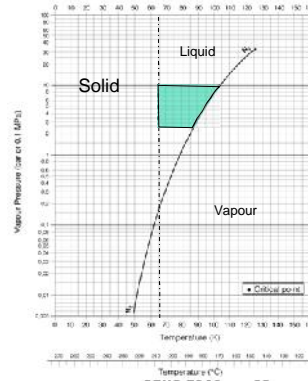
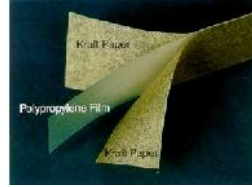
Strong increase of impedance beyond the critical current

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Cold dielectric material

1. Kraft paper for DC
 - ◆ Dielectric strength 25-50 kV/mm & $\epsilon_r = 2-5$
2. Poly Propylene Laminated Paper (PPLP) for AC
 - ◆ Low dielectric losses and can stand low cryogenic temperature
 - ◆ Dielectric strength ~ 40 to 45 kV/mm (LN2 pressure dependent) & $\epsilon_r = 2,2$
3. But also Liq N₂ under 5 to 10 bar
 - ◆ Dielectric strength ~ 40 to 80 kV/mm (pressure dependant) & $\epsilon_r = 1.4$
 - ◆ **But in N₂ gas dielectric strength only 2-3 kV/mm**
 - ◆ **∅ Gaz bubbles are forbidden ..**



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PPLP AC Losses in HV insulation

$$W_{ins} = 2 f \tan \delta C U^2$$

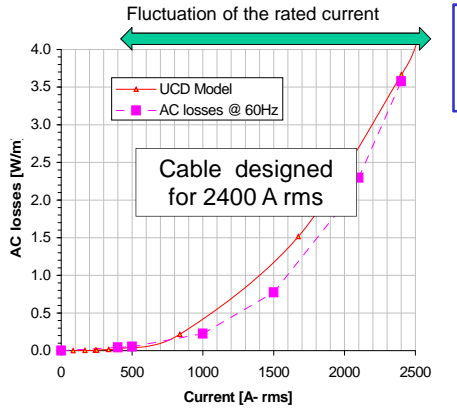
- f Frequency in [Hz] typically 50-60 Hz
- C Capacity of the cable per meter in [F/m] $C / m = 2f v_r v_0 \ln\left(\frac{r_{ext}}{r_{int}}\right)$
C ~ to 1,2 10⁻¹⁰ F/m for high voltage cable
- U V_{rms} voltage in [V] between ground and phase
- δ Loss angle from the insulation material in [°] ~0,001 to 0,002

Voltage rms	Losses W/m at 77K
63 kV	0,05-1
110 kV	0,15-0,3
220 kV	0,5-1
400 kV	2-4

Typical losses from Cryogenic envelopes ~1 to 1,5 W/m
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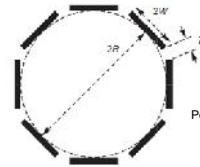
Many models exists to estimate the AC losses in assembled power cable



The AC losses are dependant on the **instantaneous** current and not the design current

Rem : If **only parralel field** is considered losses at 2400 A rms ~2,6 W/m

A limited contribution of the **perpendicular field** at the edges of tapes due to polygonal shape has to be considered !!!



Polygonal shape of the cable from Mawatari, Y. &Al




Example: UCD model & measurements
Cable core with 2 layers of Bi2223 + 1 screen




Losses at 65-80 K in cold dielectric power cables

	Dependence	Parameters	Losses at 65-77 K	Losses at RT
Cryogenic envelop losses	None	Super-insulation spacer and diameter	0,5 to 2 W/m	12,5 à 50 W/m
HTS AC losses	Transported current Magnetic field distribution	Cable design (pitches, diameter,..)	0,05 to 1 W/kA.m	1,25 to 15 W/kA.m
Dielectric AC losses	Voltage level	Capacity of the cable and material (tg δ)	Up to à 1 W/m	Up to 12,5 W/m for 220 kV
Eddy current AC losses	Magnetic field distribution	Cable design (pitches, diameter,..)	0,05 to 0,1 W/kA.m	1,25 to 2,5 W/kA.m

For a Cu cable typycal. 20 W/kA.m

Nb: For DC current, the losses are only from the cryogenic envelop

Systems	2 or 3 coaxial poles or phases	2 or 3 poles or phases in one envelop	1 pole or phase per envelop
Conception			
Voltage	For low voltage < 30 kV	Up to medium Voltage < 90 kV	For high voltage
Interests	- Reduced costs minimized the quantity of tapes - One termination for the 2 poles or 3 phases	Possibility for one termination for the 2 poles or 3 phases	-For very high power(500 MW or more) - Possibility for the longest lengths
	No environmental impact		

Systems	2 coaxial poles	2 twisted poles in one envelope	1 pole per envelope
Conception			
Voltage	Low voltage < 30 kV	Medium voltage 90 kV	Medium to high voltage > 90 kV
Benefits	Very compact cables		Very bulk power transferred up to 5 GW
	- No magnetic impact -Common terminations and joints for both poles	Common terminations and joints for both pole	Maximize unit length
	No thermal impact		

Other important parameters to consider

1. Cabling process (Multi-steps process)
 - Cabling machines \Rightarrow Tension & torsion on tapes & assembled semi-finish conductors
 - Insulation lapping machines \Rightarrow Radial pressure generated by the lapped insulation
 - Caterpillars & capstans
 - Bending on drums
2. Installation on site
 - Push & pull
 - Drum size and access
 - Turns of the cable path way
3. Thermal shrinkage
 - Shrinkage $\sim 0.3\%$ contraction between 300K to 77 K \Rightarrow 3 m per km or a stress of few tons \Rightarrow **Stress/strain management into the system is required**
 - Compatibility of the different materials

Exceptional events : The superconducting power distribution system shall survive

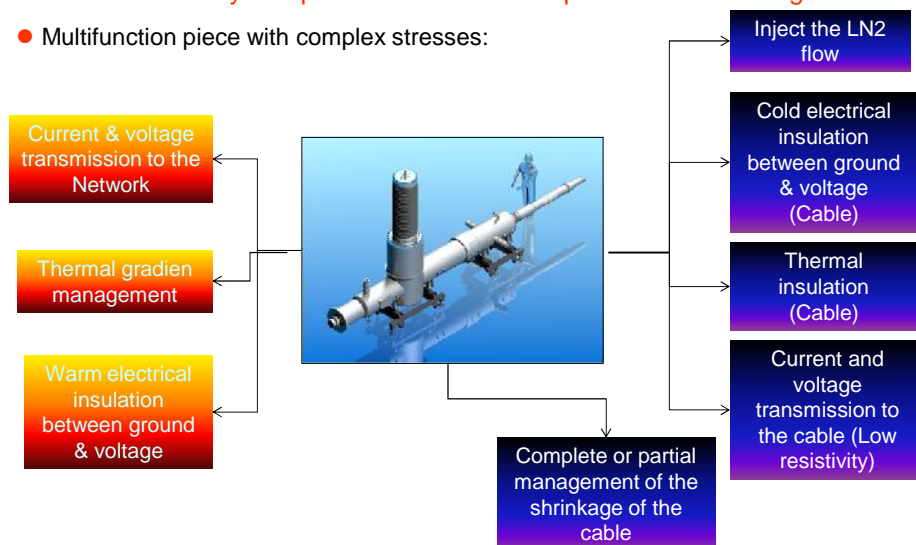
1. Fault currents
 - Very high current pulses = 10 to 50 time nominal current during the switching time of few 100 ms
 - Solution: Use copper or aluminum core to transfer the energy of the fault combined with high pressure LN₂ (3 to 10 bars) to avoid bubbles
2. Impulse voltage
 - Lightning voltage pulses = few hundreds to million of kV during a few ms
 - Tested with a HV pulse (HT increase 1,2 ms / HT decrease 50 ms)
 - Switching voltage pulses = few hundreds of kV during a few ms
 - Tested with a HV pulse (HT increase 250ms / HT decrease 2500 ms)
 - Solution: Use high pressure LN₂ (3 to 10 bars) to avoid bubbles in HV insulation
3. Over-voltage
 - High voltage pulses (few % more than rated voltage)
 - Solution: Design of the cable with a sufficient insulation thickness to meet safety requirements

Introduction to superconducting power cable systems

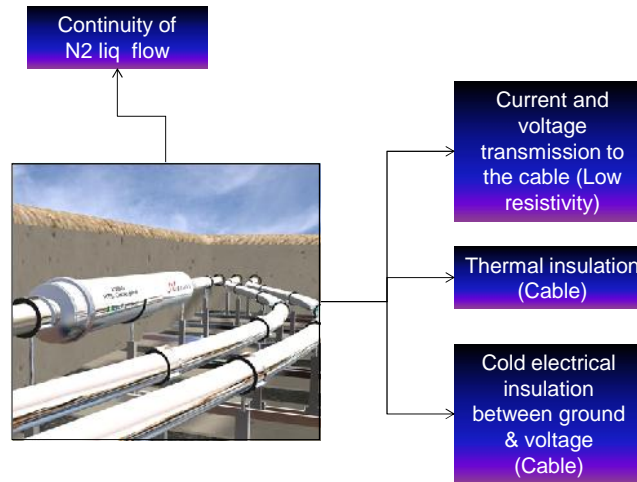
1. The 5 main components
 - A. Superconducting tapes and wires
 - B. Cryogenic envelopes
 - C. Cryogenic machines
 - D. Cable designs
 - Warm dielectric
 - Cold dielectric
 - E. Terminations & Joints
2. Tests & Reliability
3. Some applications
4. HTS power cable system benefits

■ Termination: a key component to connect the power cable to the grid

- Multifunction piece with complex stresses:



- Joint: Cold electrical connection for long cables on field

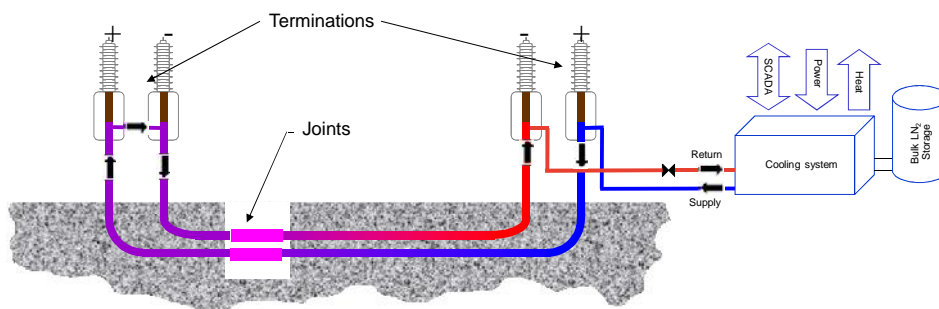


- Cryostat losses
 - Depending on the size from 1 to 5 W at 77K)
- For current leads a balance between
 1. Thermal conduction of the current leads for termination
 2. Electrical resistance of the current leads
- Electrical & resistive connections of the cable
 - Core & screen

W/kA	77K	RT
Termination when energized	40 à 50 W/kA	0,8 to 1 kW/kA
Termination When I tr=0	20 to 25 W/kA	0,4 to 0,5 kW/kA
Joint ~1 μ Ω	1	20 W

1. Terminations: can be tested in lab before field installation
2. Field Joint: tests only on prototypes

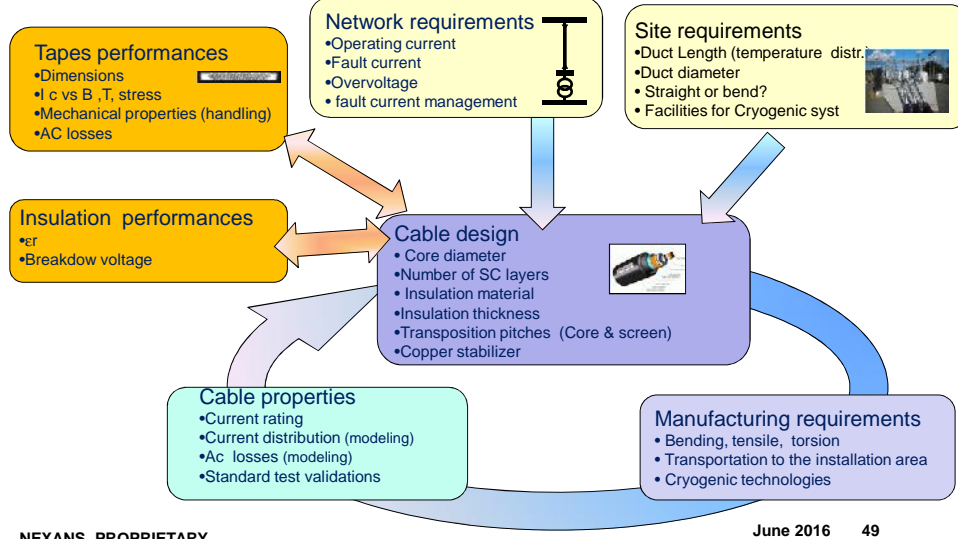
- Failures generally come from:
 - ◆ Thermal stresses and fatigue
 - ✓ Thermo-mechanical modeling
 - Differential shrinkage
 - Cooling rates
 - ✓ Materials properties to be measured on prototypes (thermal expansion coefficient, thermal conduction,...)
 - ◆ Aging of dielectric materials
 - ✓ Only few data on the materials used
 - but low temperature (77K) will help to limit aging phenomena
- ⇒ To be qualified by cooling down several times on the final terminations & joints



1. The coolant can be gaseous or liquid
2. Temperature difference and pressure drop between inlet and outlet depend on:
 - Length of the cable
 - Thermal and electrical losses

⇒ For optimized system this temperature difference < 2 K and pressure drop less than 3-5 bars

- Electro-magnetic optimization for : **the highest current** (optimum magnetic field on tapes) **with the highest efficiency** (reduction of costs of cryogenic systems)

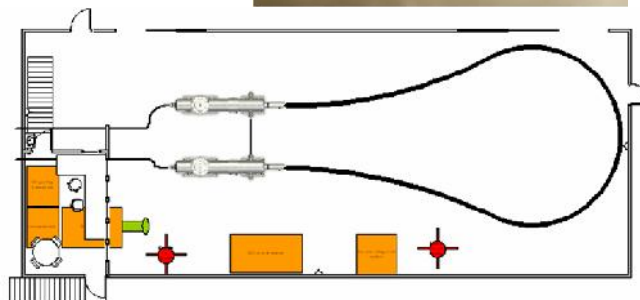


Introduction to superconducting power cable systems

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1. Reliability & long time test programs are running
 - LIPA cable is in the Long Island network since april 2008
 - Southwire cable energized in august 2006
 - Fujikura cable is running long time tests with CREPRI
 - Ampacity cable runs since 2014
2. Standard tests similar as for « resistive » HV cables
 - Over-voltage tests
 - Accelerate “aging” experiments
 - ✓ Over voltages & currents
 - Long time validations on plateforms
 - New standard under preparation for AC cables based on CIGRE works

- Faraday cage de 30 m x 12 m x 9 m supply with presurized Liq N2



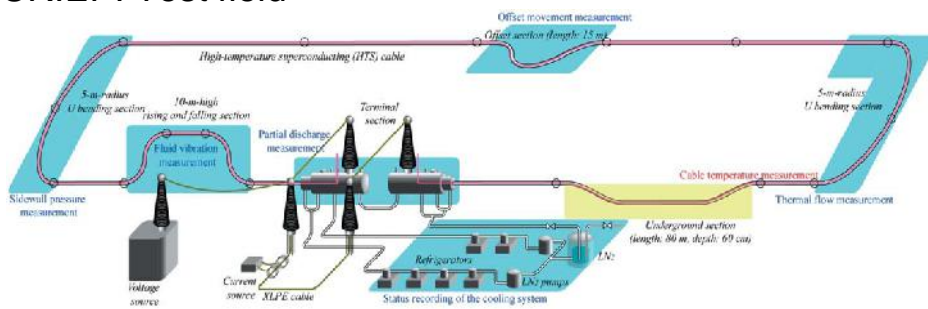


138 kV, 2400 A, 30 m Prototype in the test field in Hanover

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CRIEPI Test field



Test field for the different cases of installation

1. Tension: 77 kV
2. Current: 1kA



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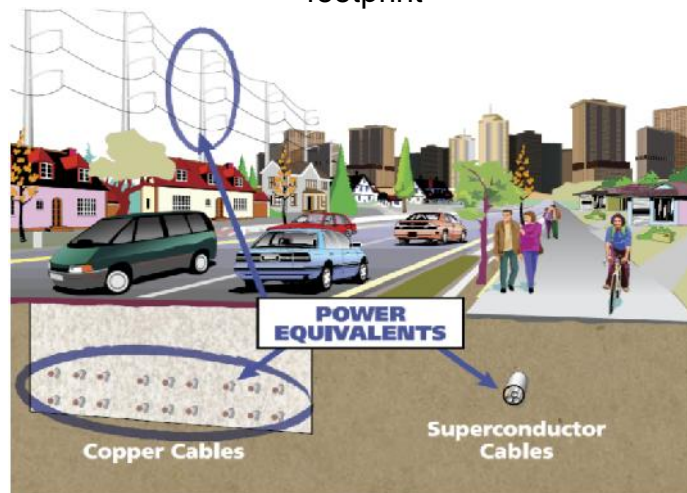
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Introduction to superconducting power cable systems

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1- Urban grids

In urban grids, superconducting cables only need a reduced footprint

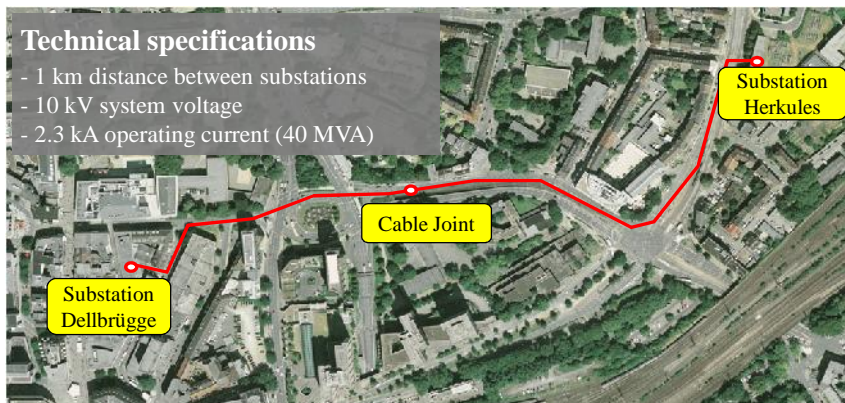


1. Urban grids: Ampacity project at Essen (1)



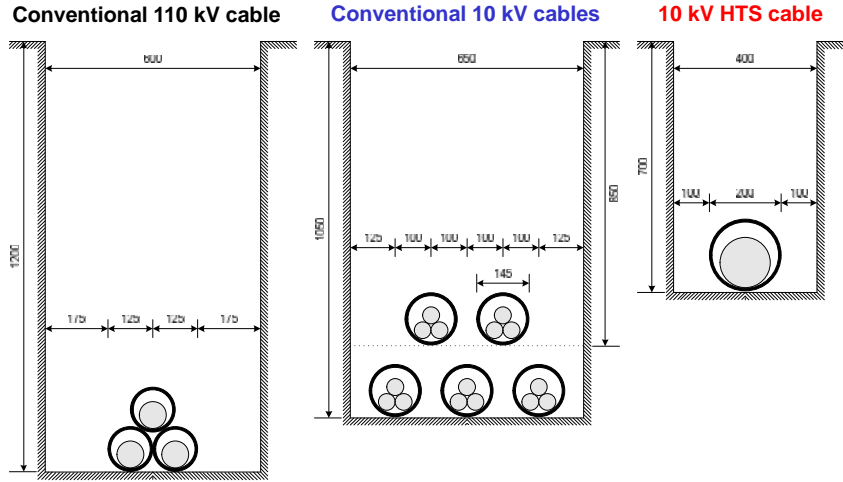
- **Application:**
Feeding the center of Essen at medium voltage (10 kV) level with a superconducting cable
- **Economic viability:**
The higher cost of the superconducting cable is compensated by savings in substation equipment
- **Additional benefit:**
Real estate becomes available in the city center

1. Urban grids: Ampacity project at Essen (2)



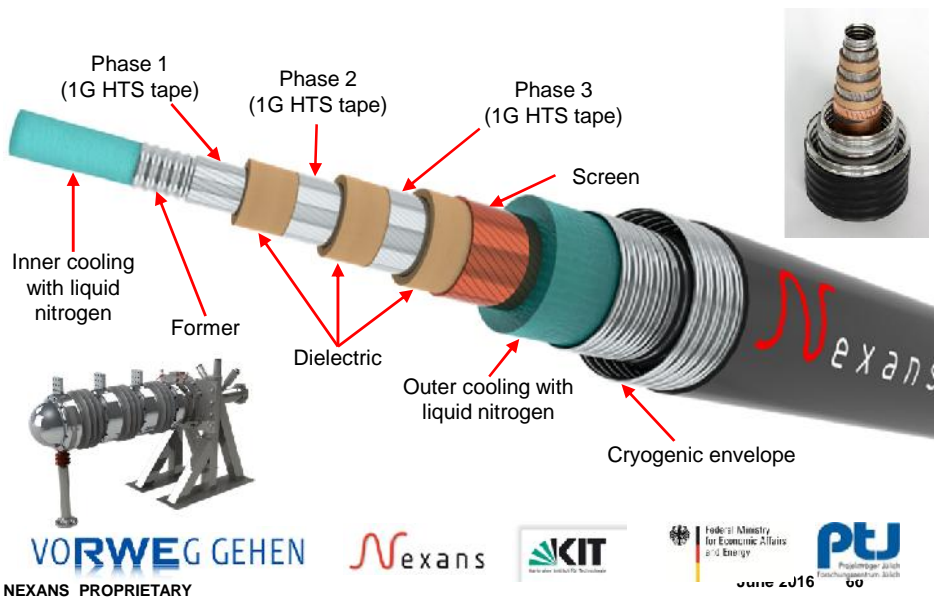
Longest high temperature superconducting (HTS) cable in the world

3 solutions considered



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1. Urban grids: Ampacity project at Essen

Official celebration on April 30, 2014

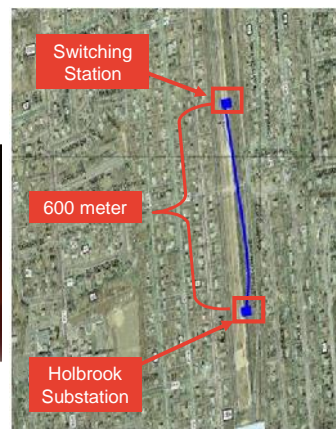


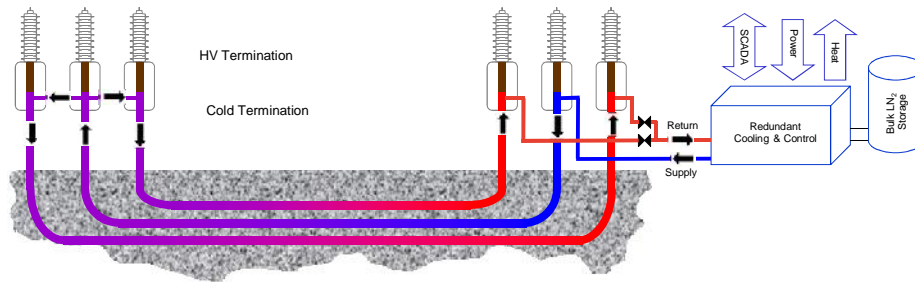
From left to right: Dr. Joachim Schneider, CTO RWE Deutschland AG, Dr. Arndt Neuhaus, CEO RWE Deutschland AG, Peter Terium, CEO RWE AG, Reinhard Paß, Lord Mayor of the City of Essen, Dr. Johannes Georg Bednorz, Nobel laureate 1987, Dr. Hans-Christoph Wirth, German Federal Ministry for Economic Affairs and Energy, Hannelore Kraft, Prime Minister of the German federal state North Rhine-Westphalia, Christof Barklage, CEO Nexans Deutschland GmbH, Prof. h.c. Dr. Joachim Knebel, area manager Karlsruhe Institute for Technology

2. Urban HV grids: LIPA project at Long Island

Demonstrated the feasibility of HV superconducting cables

- Partners: American Superconductor (leader), Long Island Power Utility (LIPA), Air Liquide
- Funding: U. S. Department of Energy
- 600 m long cable system
138kV/2400A ~ 574MVA
- Design fault current:
51 kA @ 12 line cycles (200ms)
- Cable phases pulled in underground polyethylene conduits

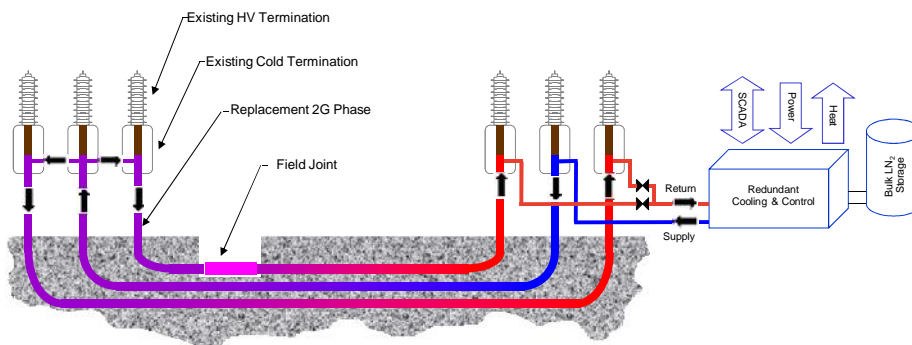




Cable successfully energized on April 22, 2008



World's longest HTS cable (at that time) successfully energized on April 22, 2008



- Project objectives
 - Thermal contraction inside the cable
 - Cable joint development
 - Repairable cryostat
 - Use of 2G wire
 - Development of modular refrigeration unit
- in March 2012
 - w Single phase of stabilized 2G cable to survive short circuit currents
 - w New cryostat (2 pieces)
 - w Cable joint

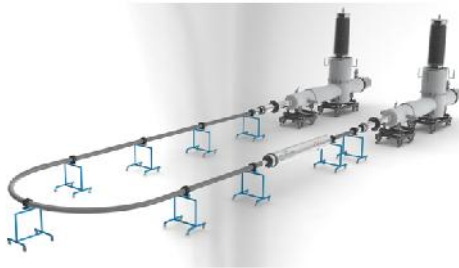


2. Urban HV grids: LIPA 2 project at Long Island

Some applications

HVAC cable joint developed and installed in field

- 138 kV HTS cable joint has been developed and qualified in a type test sequence on such small loop



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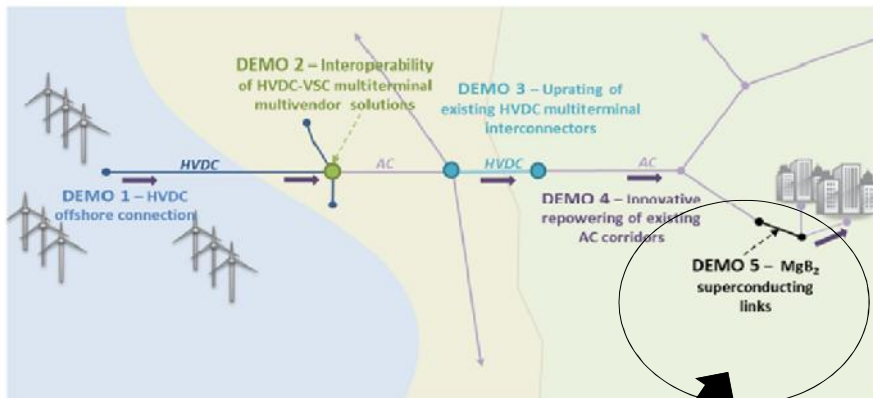
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3. HVDC grids: Bestpaths FP7 Project

Some applications

5 high level demonstration projects



 October 2014
 September 2018
  Total budget (EC contribution: 57 %)
 62.8 M€ = M\$ 70.8 = 460 M

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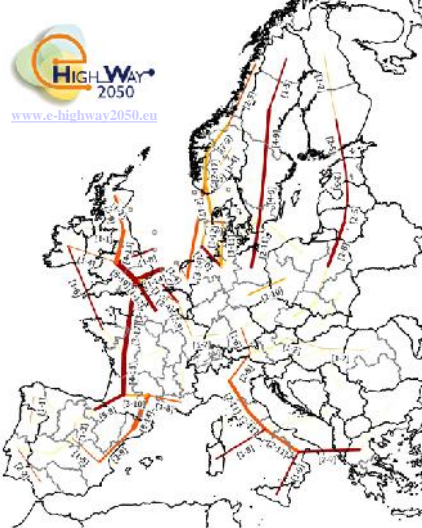
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Future prospects of transmission grid development

- **European eHighWay2050**
Project brings very useful input data
 - New methodology to support grid planning
 - Focusing on 2020 to 2050
 - To ensure the reliable delivery of renewable electricity and pan-European market integration
 - Five extreme energy mix scenarios considered

- **Whatever the scenario, 5 to 20 GW corridors are identified**
 - Major North-South corridors are necessary
 - Connections of peninsulas and islands to continental Europe are critical

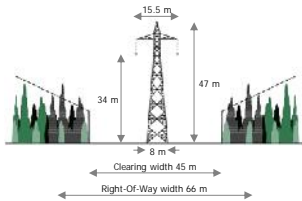
- **How to transmit more than 4 GW on long distance?**



How transmit bulk power 3-5 GW? (examples of corridors)



Nelson River DC line (Canada)
1600+1800 MVA (+2000 under construction)



Gas Insulated Lines

Geneva, Palexpo Link 2001,
470 m, 220 kV / 2 x 760 MW



XLPE cables

Raesfeld (380 kV AC, Germany)
2x 1800 MW



Frankfurt Airport,
Kelsterbach Link 2012,
900 m, 400 kV / 2 x 2285 MW



10 partners for Demo 5



Optimization of MgB₂ wires and conductors
Cable system
Cryogenic machines
Testing in GHe
Integration into the Grid



Optimization of MgB₂ wires and conductors
Cable system



MgB₂ wire
Optimization of MgB₂ wires and conductors



Cryogenic machines



Reliability
Integration into
Transmission grid



Cable system
Integration into
Transmission grid
Testing in GHe
Reliability



Scientific coordination
Dissemination &
exploitation



Cable system



Cable system

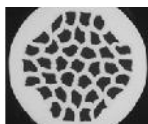


Cable system

Main objectives of the superconducting demonstrator

- 10 partners to demonstrate the following objectives
 - Demonstrate full-scale **3 GW** class HVDC superconducting cable system operating at 320 kV and 10 kA
 - Validate the novel **MgB₂** superconductor for high-power electricity transfer
 - Provide guidance on technical aspects, economic viability, and environmental impact of this innovative technology

Process development to manufacture a large quantity of high performance MgB₂ wires at low cost

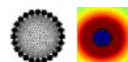


Cable and termination development + manufacturing processes



Validation of cable operations with laboratory experiments performed in He gas at variable temperature

Operating demonstration of a full scale cable system transferring up to 3.2 GW



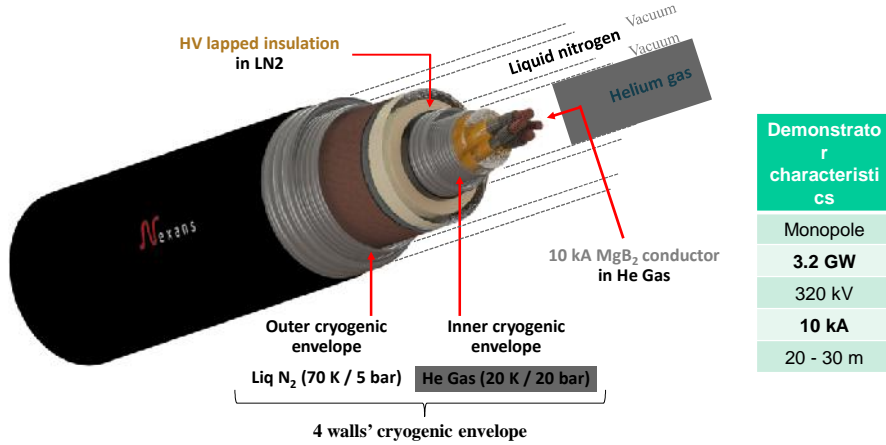
System integration pathways for HDVC applications

Investigation in the availability of the cable system

Preparation of the possible use of H₂ liquid for long length power links

Superconducting HVDC cable concept Conceptual design

- Two fluids to guaranty the safety of the operation



Demonstrator characteristics
Monopole
3.2 GW
320 kV
10 kA
20 - 30 m

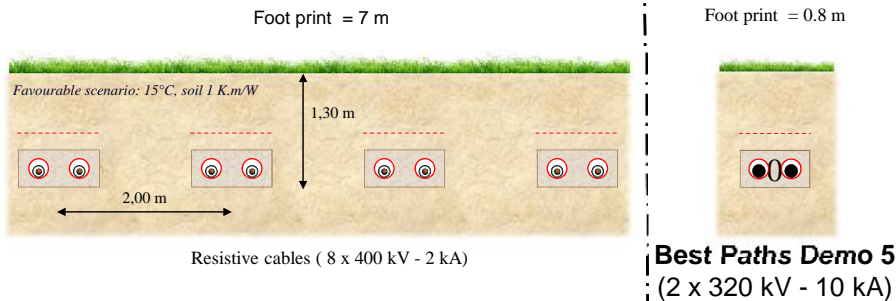
Project on going....

Reduced space for cable installation and substations

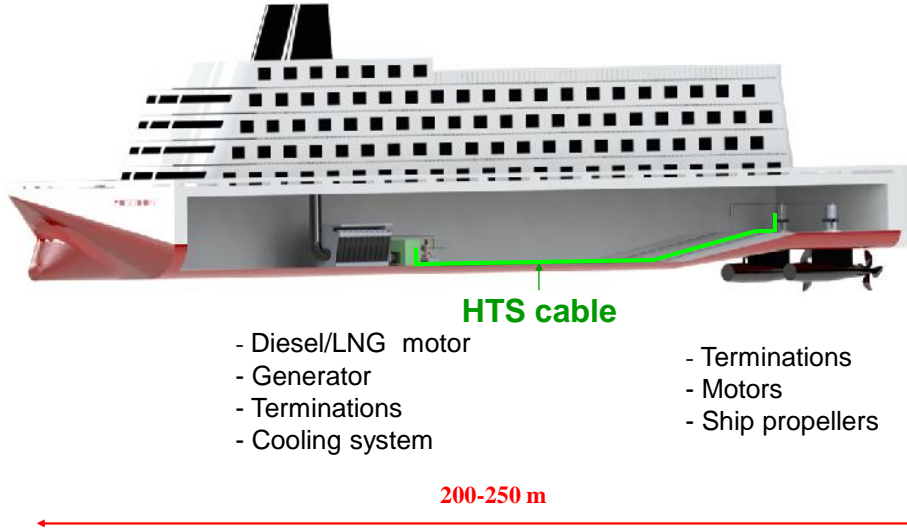
Significant reduction of right-of-way and excavated soil

No thermal dependence to the environment

Example: 6.4 GW DC power link with XLPE cables

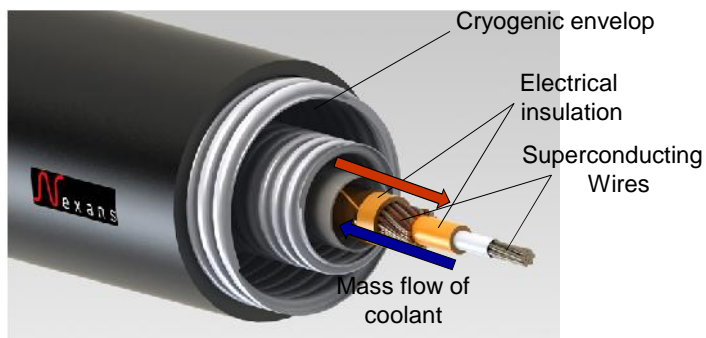


Project on-going....To be tested in 2017



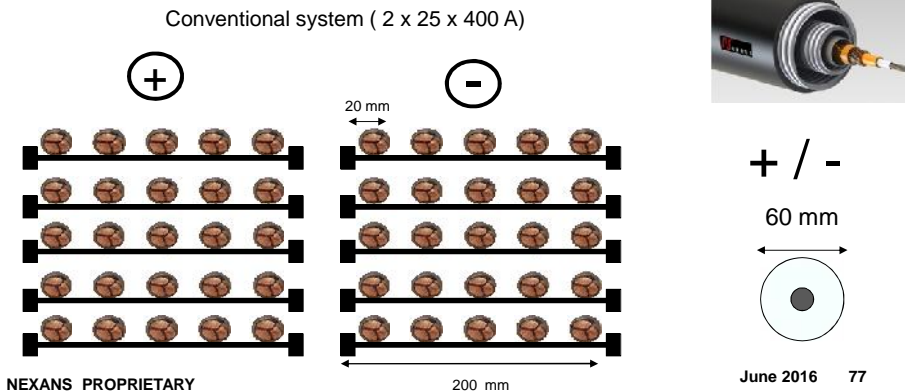
Date et page : 75

1. Distribution of high power possible at low voltage (<4 kV)
2. Reduction of the losses for distributed power $P > 5\text{MW}$



4. HTS cables onboard a ship

- 3. No environmental impact (*thermal or electromagnetic*)
- 4. Very compact and light cable
 - ◆ D ext = 60 mm for bifilar SC cable 66 MW 10 kA/3,3 kV
 - ◆ Cryogenics system footprint between 1 to 5 m²



4. HTS cables onboard a ship

- 1. Large commercial electrical ships (*several electrical motors P > 5 MW*)

- Cruise ships
- Container cargos
- LNG tankers
 - ◆ Large cooling power available on board
 - ◆ Habilitation for operation in cold environment
- FPSO (Floating production storage and offloading)



- 2. Navy ships
 - Degaussing cables (ex USS Higgins)
 - Submarines



The electrical or hybrid plane will allow to reach the objective of 50% CO₂ reduction per passenger in 2020

■ From 5 to 100 MW are necessary to power the plane according to the number of passagers



Voltair project from Airbus ind.

Up to 95 % of weight reduction
with superconducting cables !!!



Ex: Cable 1,2 MW
U_{op}= 200 V, I_{op} = 2 x 3000 A
Weight < 6 kg/m (<1kg/km.A)
(140 kg/m for equivalent copper
cables)

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All activities requiring large electrical power at low voltage such as:

- Data centers
- Metallurgy plants
- Harbor and off shore platforms
- Railways
- Large reviewable energy farms
-

can potentially benefit from superconducting cable technologies...

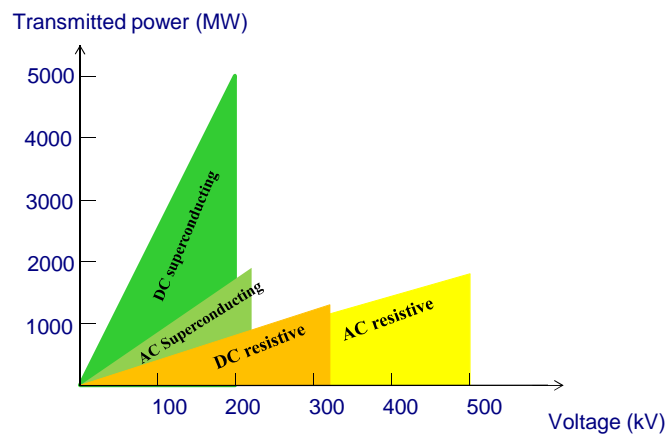
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3. Different projects
4. HTS power cable system benefits

HTS power cable system benefits (1)



HTS cables provide a much higher power transfer capability at the same voltage

1. Increased power transferred at a reduced voltage level
2. Negligible thermal impact on the environment
3. No outer magnetic field during normal operation
4. Reduce volume of raw materials required
5. Reduced space for cable installation and substations
 - Easier cable installation
 - Increase the possibilities of electrification

1. Superconducting cables are a new tool to adapt the electrical network and improve the efficiency in a world becoming increasingly urban with a production of electricity less centralized.
2. All the elements are ready to build superconducting links adapted to many applications for the environmental challenges of tomorrow
3. Superconducting cables are vectors of the energy transition required for our future
4. But still a lot of technical and commercial works is needed for an optimized use and general acceptance.....



**Thank you
for your
attention !**

Cartoon by
Thomas Kodenkandath
(The Week, 1988)