

Discontinuity lines in Nb thin films with artificial border micro-indentations

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Ref: J. Brisbois, O.-A. Adami, J. I. Avila, M. Motta, W. A. Ortiz, N. D. Nguyen, P. Vanderbemden, B. Vanderheyden, R. B. G. Kramer, A. V. Silhanek, PRB **93**, 054521 (2016)

Defects in superconductor films

- **Defects** play a key role in type II superconductors acting as **pinning sites** for vortices, allowing dissipation-less current transport in the mixed state.
- Defects in the borders generate long range regions where the **current changes direction** abruptly: the discontinuity or *d-lines*.

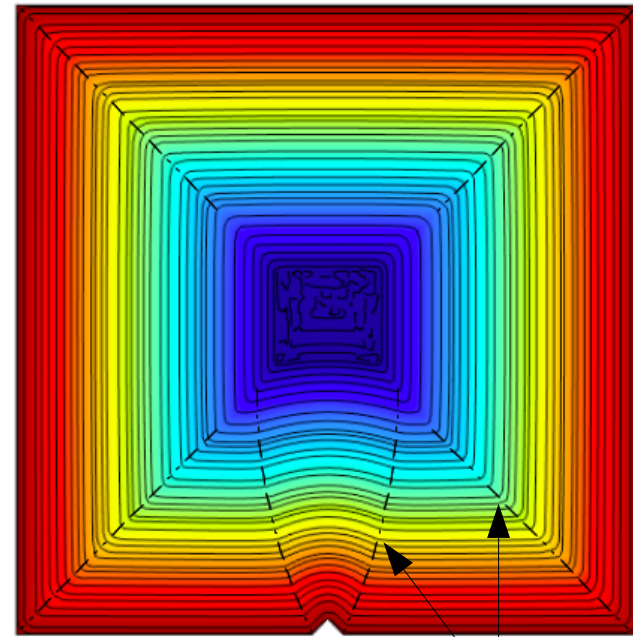
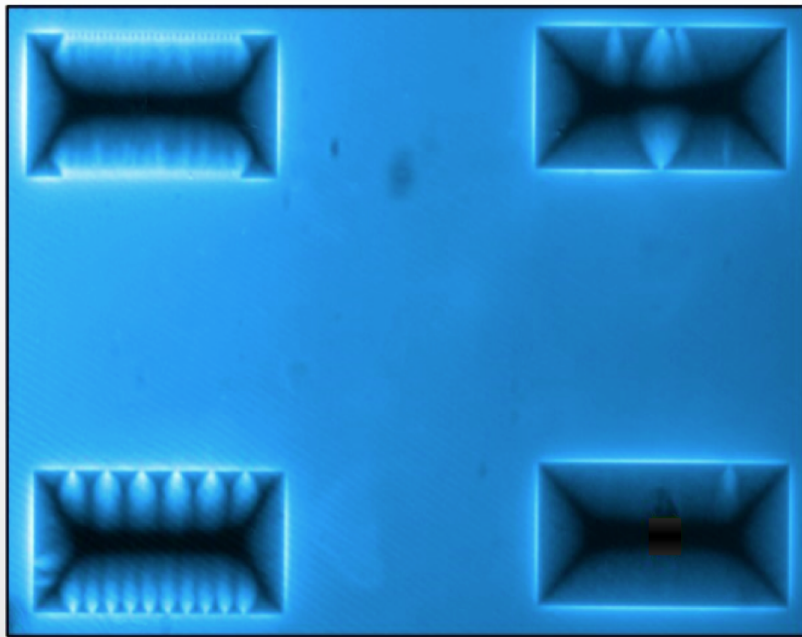


FIG.11: Left, Magneto-optical image of thin film samples with defects, Right: representation of d-lines

Simple current model: current has uniform magnitude j_c

Simple d-lines model: d-lines are equidistant from 2 nearest straight edges. For semi-circular and triangular defect of height R , its associated d-line will be (BB model):

$$y \approx \frac{x^2}{2R} - \frac{R}{2} \quad (\text{I1})$$

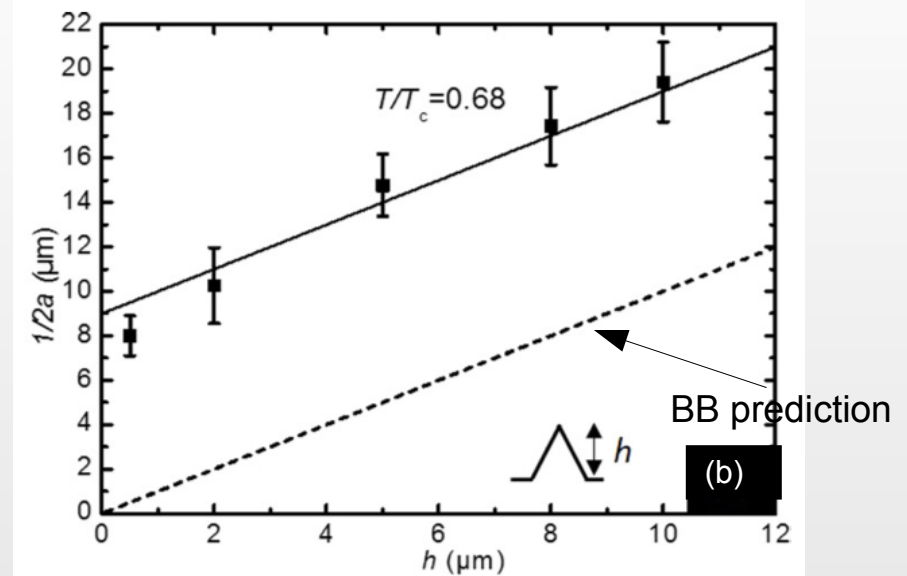
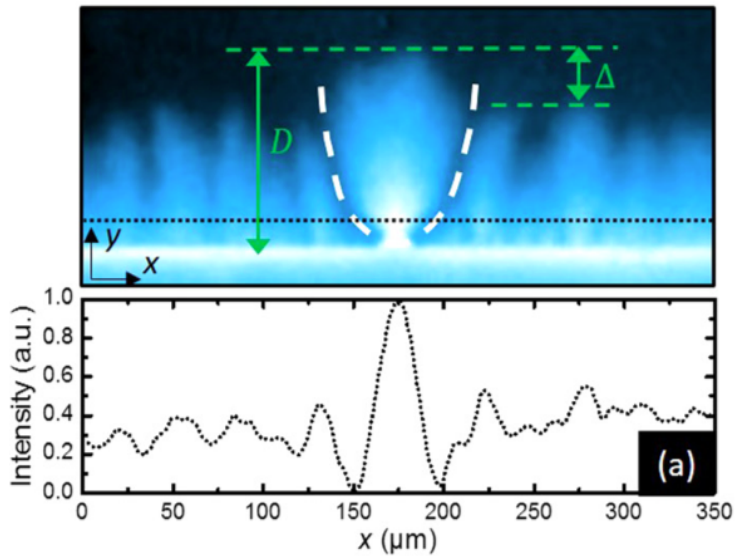


FIG.12: (a) upper flux penetration in triangular indentation of 10 μ m height and lower intensity profile along dotted line. (b) 1/2a vs triangular defect height, where parameter 'a' is obtained from d-line shape fit $y=ax^2+b$

From Eqn (I1)

$$\frac{1}{2a} = R = h \quad (\text{I2})$$

Experimental values much higher than predicted!

-Calculating the magnetic field distribution of a 2D superconductor in the mixed state. Two cases: Local and Non-Local

Local or longitudinal case:

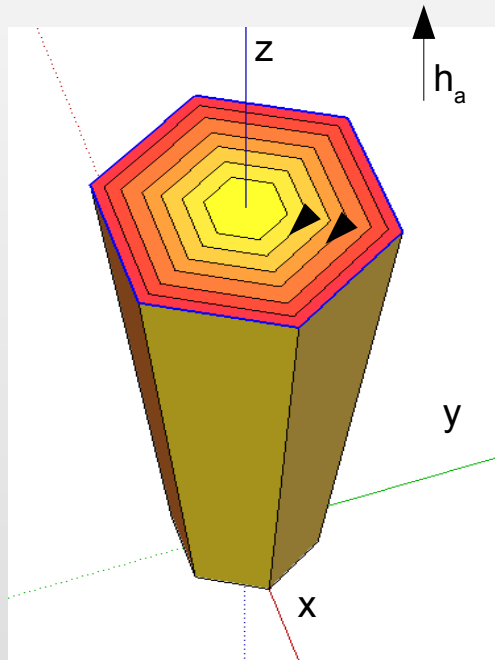


FIG.1

Neglecting displacement currents, Maxwell eqns are:

$$\mathbf{j} = \nabla \times \mathbf{H} \quad (1)$$

$$\mu_0 \frac{\partial \mathbf{H}}{\partial t} = -\nabla \times \mathbf{E} \quad (2)$$

Replacing (1) in the constitutive relationship, and replacing in (2):

$$\mathbf{E} = \rho \mathbf{j} = \rho \nabla \times \mathbf{H} \quad (2)$$

$$\mu_0 \frac{\partial \mathbf{H}}{\partial t} = -\nabla \times (\rho \nabla \times \mathbf{H}) \quad (3)$$

Because of the symmetry, the currents must be planar, and therefore \mathbf{H} must point in the z direction and be independent of z :

$$\mathbf{H} = (h(x, y, t) + h_a(t)) \hat{z} \quad (4)$$

$$\rho = \rho(x, y) \quad (5)$$

$$\frac{\partial h}{\partial t} = \nabla \cdot (\rho \nabla h) / \mu_0 - \frac{\partial h_a}{\partial t} \quad (6)$$

Boundary condition $h=0$

Integrated in COMSOL
Multiphysics

It follows that h is also a current stream-function, since:

$$\mathbf{j} = \nabla \times (h \hat{z}) \quad (7)$$

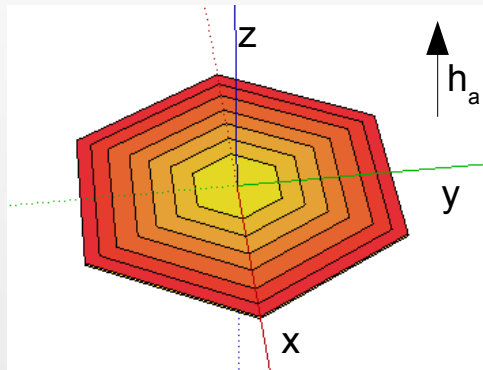
And then
$$j = |\mathbf{j}| = |\nabla \times (h \hat{z})| = |\nabla h| \quad (8)$$

Ref: E. H. Brandt, PRB **52**, 21 (1995), 15442

Magnetic field in thin film: non-local or transversal case

Introducing the sheet current:

$$\mathbf{J} = d \mathbf{j} \quad (12)$$



Where d is the thickness of the film, and introducing the stream function g :

$$\mathbf{J} = \nabla \times (g \hat{\mathbf{z}}) \quad (13)$$

FIG.3

The current induced field H_d time derivative is now given by:

$$\frac{\partial H_d}{\partial t} = \iint Q(r, r') \frac{\partial g(r')}{\partial t} dS', \quad \text{with} \quad (14)$$

$$Q(r, r') = \lim_{z \rightarrow 0} \frac{1}{4\pi} \frac{2z^2 - R^2}{(z^2 + R^2)^{5/2}}, \quad R = |\mathbf{r} - \mathbf{r}'| \quad (15)$$

And the equation for the time evolution of g is given by:

$$\nabla \cdot (\rho \nabla g) / d \mu_0 = \frac{\partial H_a}{\partial t} + \frac{\partial H_d}{\partial t} \quad (17)$$

$$\nabla \cdot (\rho \nabla g) / d \mu_0 = \frac{\partial H_a}{\partial t} + \iint Q \frac{\partial g}{\partial t} \quad (18)$$

Implemented
in Matlab

Integration of eqn (18) is not trivial as $\partial g / \partial t$ is inside the integral.
Here an algorithm based on space Fourier transforms (F) was used.

$$\frac{\partial H_d}{\partial t} = \iint Q(\mathbf{r} - \mathbf{r}') \frac{\partial g}{\partial t}, \text{ apply } F() \quad (19)$$

$$F\left(\frac{\partial H_d}{\partial t}\right) = F\left(\iint Q(\mathbf{r} - \mathbf{r}') \frac{\partial g}{\partial t}\right) = \frac{k}{2} F\left(\frac{\partial g}{\partial t}\right) \quad (20)$$

$$\frac{\partial g}{\partial t} = F^{-1}\left(\frac{2}{k} F\left(\frac{\partial H_d}{\partial t}\right)\right) \quad (22)$$

$$\frac{\partial g}{\partial t} = F^{-1}\left(\frac{2}{k} F\left(\nabla \cdot (\rho \nabla g) / d - \frac{\partial H_a}{\partial t}\right)\right) \quad (23)$$

Where it was used that the Fourier transform of $Q(\mathbf{r} - \mathbf{r}')$ is $k/2$

Ref: J I Vestgård, P Mikheenko, Y M Galperin, T H Johansen, *New Journal of Physics* 15 (2013) 093001

-What about the resistivity?

In a type II superconductor, the resistivity above H_{c1} can be modeled by:

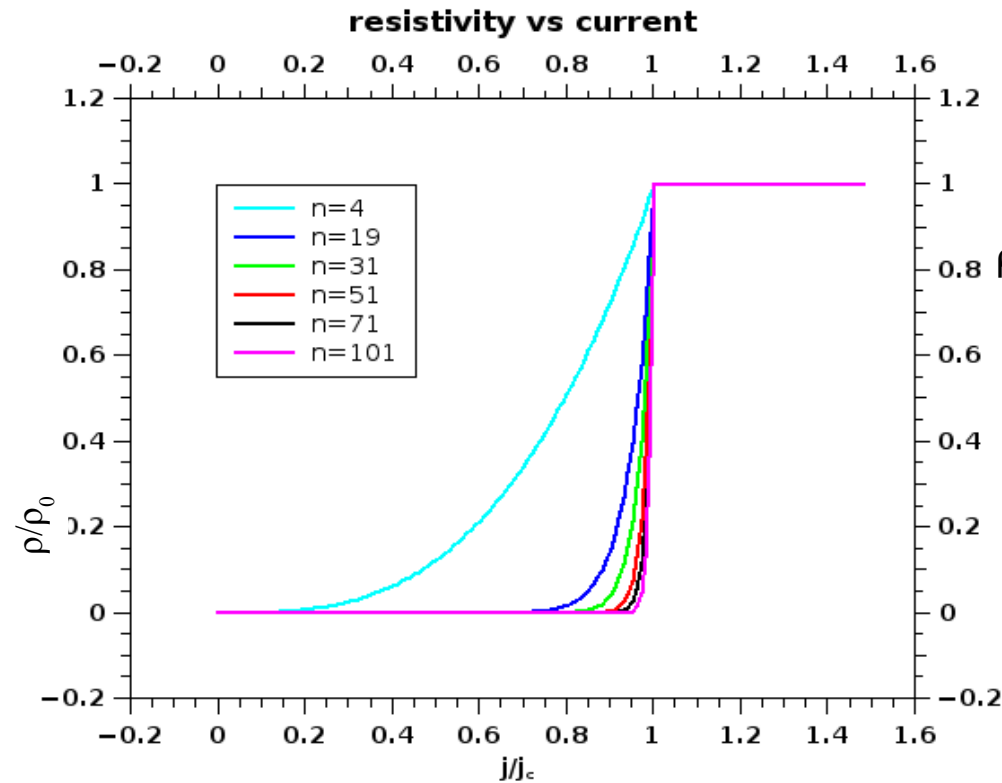


FIG.2: Resistivity vs current for different creep exponents for $T < T_c$

MODEL 1: constant j_c

$$\rho = \begin{cases} \rho_0 |\nabla h / j_c|^{n-1}, & \text{for } |\nabla h| < j_c, T < T_c \\ \rho_0, & \text{for } |\nabla h| > j_c, T < T_c \\ \rho_n, & \text{for } T > T_c \end{cases}$$

(9)

Where j_c is the critical current, and n is the creep exponent.

Taking a magnetic field dependent critical current:

$$j_c = j_{c0} \left(\frac{H}{H_{c2}} \right)^{-\gamma} \quad (10)$$

Wide range of $0 < \gamma < 1.9$ in literature, here used 0.37 from experimental fit

MODEL 2

$j_c = j_c(H)$:

$$\rho = \begin{cases} \rho_0 \left(\frac{H}{H_{c2}} \right)^{\gamma(n-1)} |\nabla h / j_{c0}|^{n-1}, & \text{for } T < T_c \\ \rho_n, & \text{for } T > T_c \end{cases} \quad (11)$$

Calculations summary:

400 μm x 400 μm , 10 μm height, 20 μm base
triangular defect

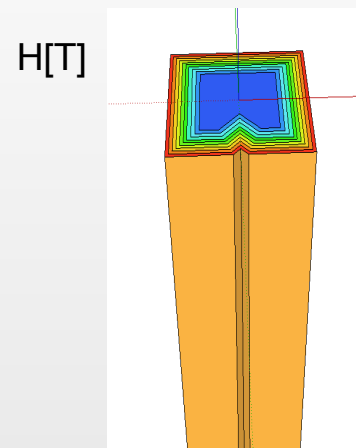
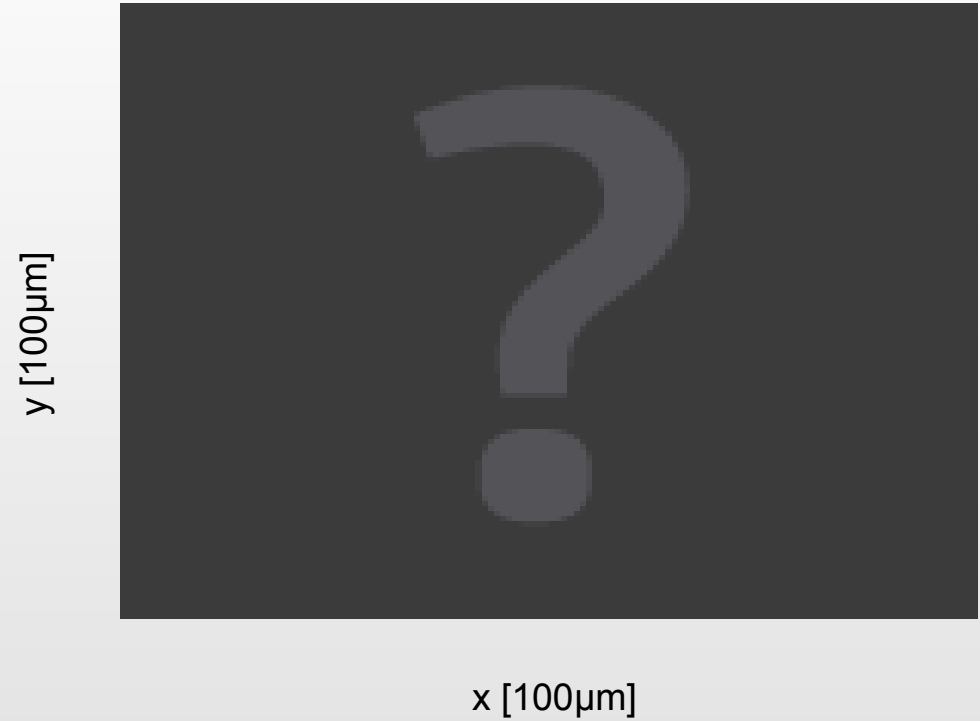
Constant field rate 10^{-3} T/s

1) Local or longitudinal case considering
constant j_c

2) Non-local or transversal case considering
constant j_c

3) Non-local or transversal case considering
 $j_c = j_c(H)$

Results



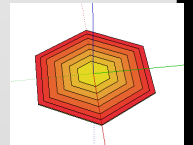
ANIM.1: Local case: d-line under external field ramp of 0.001 T/s. $N=51$, $\rho_0=10^{-14}$ Ωm , $j_c=10^{10}$ A/m². Triangular defect of 20μm base and 10μm height.

y [100 μ m]



H[T]

x [100 μ m]



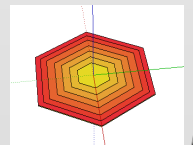
ANIM.2:Non-Local MODEL 1: d-line under external field ramp of 0.001 T/s. $N=51$, $\rho_0=10^{-14}$ Ω m, $j_c=10^{10}$ A/m², $d=100$ nm. Triangular defect of 20 μ m base and 10 μ m height.

y [100 μm]



H[T]

x [100 μm]



ANIM.3: Non-Local case MODEL 2: d-line under external field ramp of 0.001 T/s.
 $N=51$, $\rho_0=1.57 \times 10^{-7} \Omega\text{m}$, $j_{c0}=1.36 \times 10^9 \text{ A/m}^2$, $H_{c2}=1.625\text{T}$, $d=100\text{nm}$, triangular defect
of 20 μm base and 10 μm height.

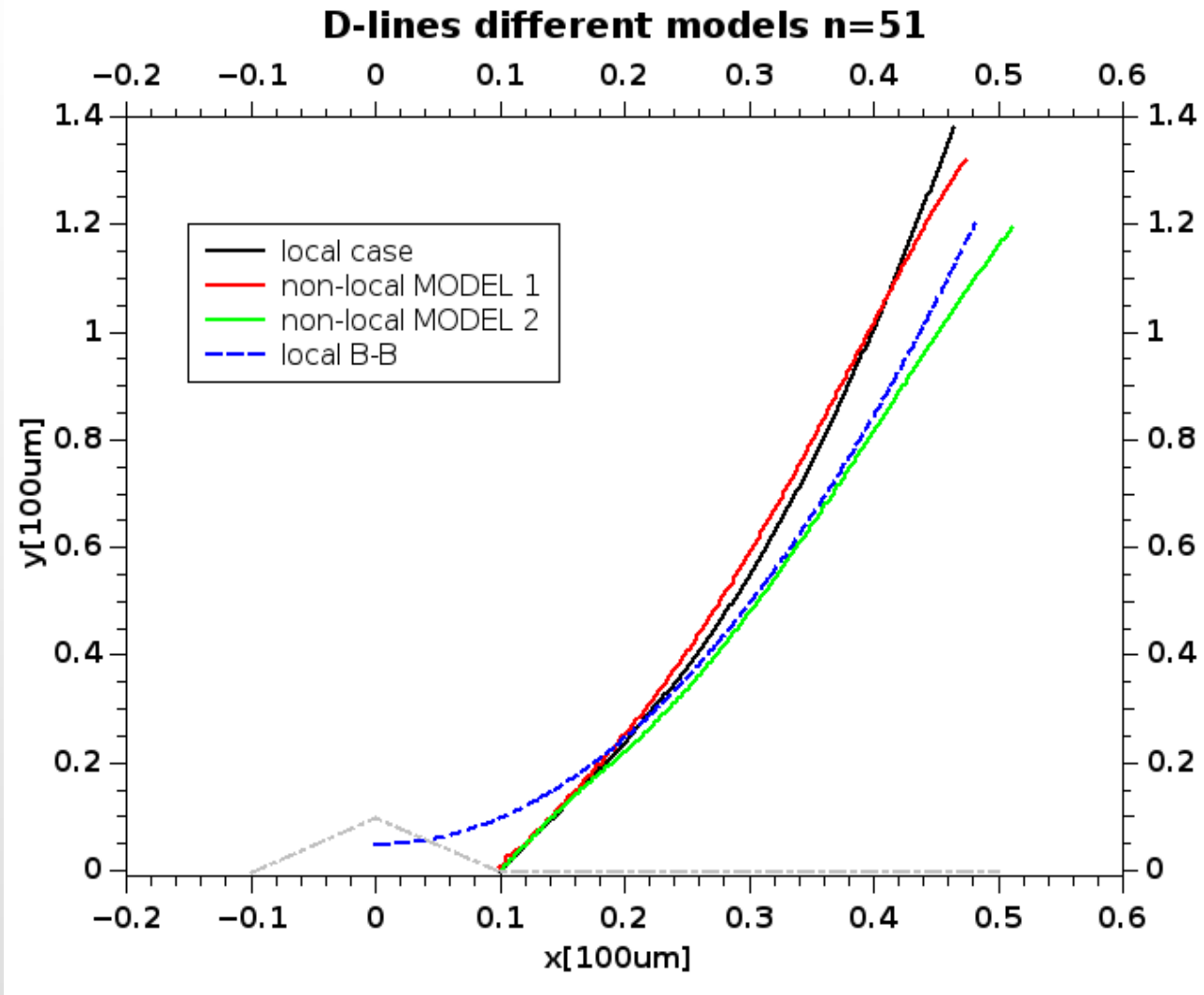


FIG.5: D-lines for previous configurations + bean model prediction

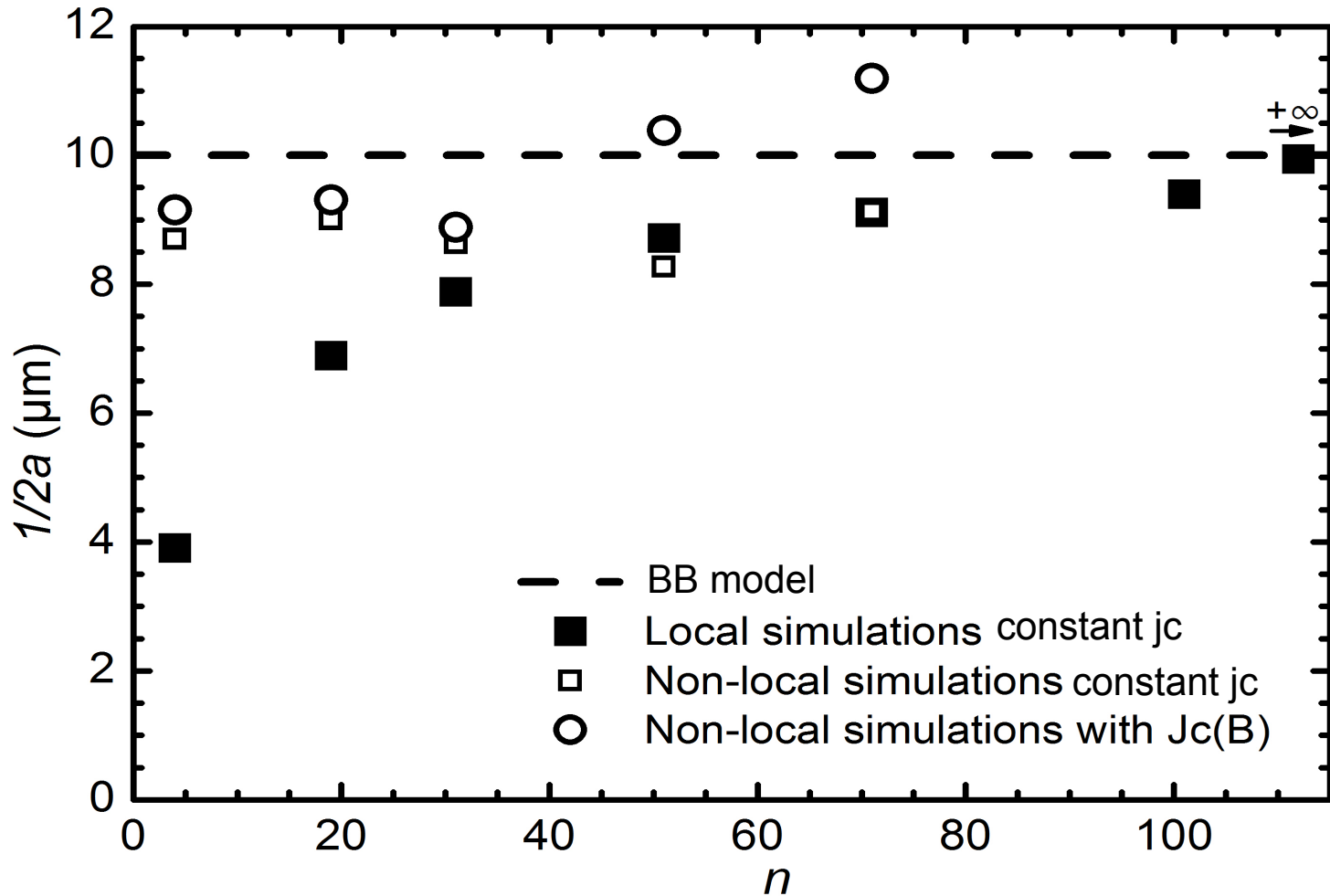


FIG.6: Graph $1/2a$ vs n for different models, obtained from second order fit of d-lines $y=ax^2+const.$

Conclusions

Resistivity model is relevant as it modifies the dynamics of magnetization and therefore the shape of d-lines.

$j_c = j_c(H)$ provide $1/2a$ values higher than BB model, in better accordance with experimental measurements.

Necessary to include other parameters like temperature variations

Acknowledgements

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